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# **NUMERICAL SIMULATION OF FREE-SURFACE LIQUID LITHIUM FLOWS IN TOKAMAK TOROIDAL GEOMETRY**

ROBERT D. WOOLLEY

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## **BACKGROUND**

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**A LIQUID LITHIUM WALLS ELECTROMAGNETIC CONFINEMENT conceptual idea was presented at first APEX meeting:**

**CONFINE A THICK (1+ METER) FLOWING LIQUID LITHIUM LAYER BY ELECTROMAGNETIC AND CONTACT FORCES TO ENCLOSE A TOROIDAL MAGNETICALLY CONFINED PLASMA.**

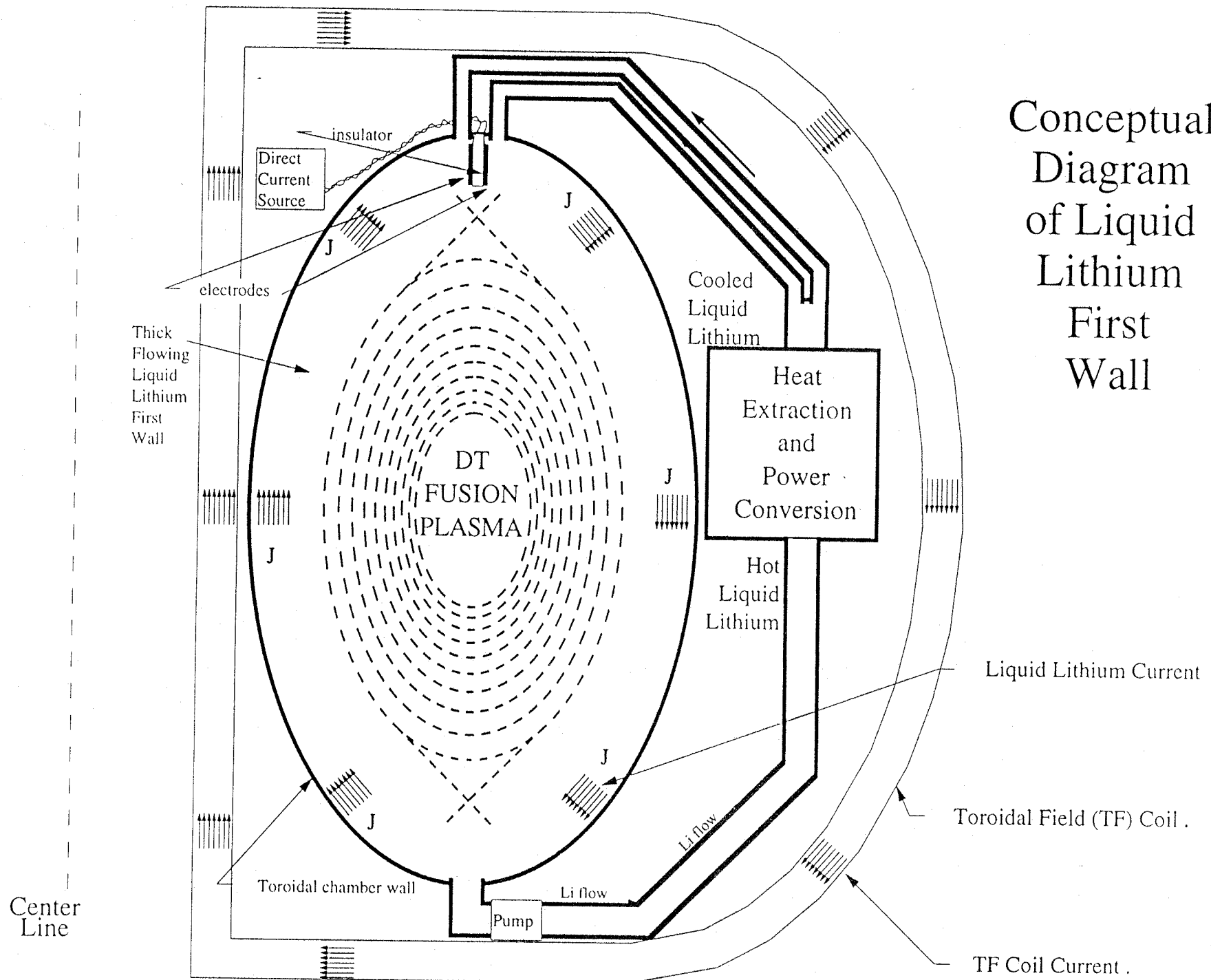
**This is analogous to an extra TF coil turn, but of flowing liquid lithium.**

**Two axisymmetric streams of liquid lithium enter top of toroidal chamber.**

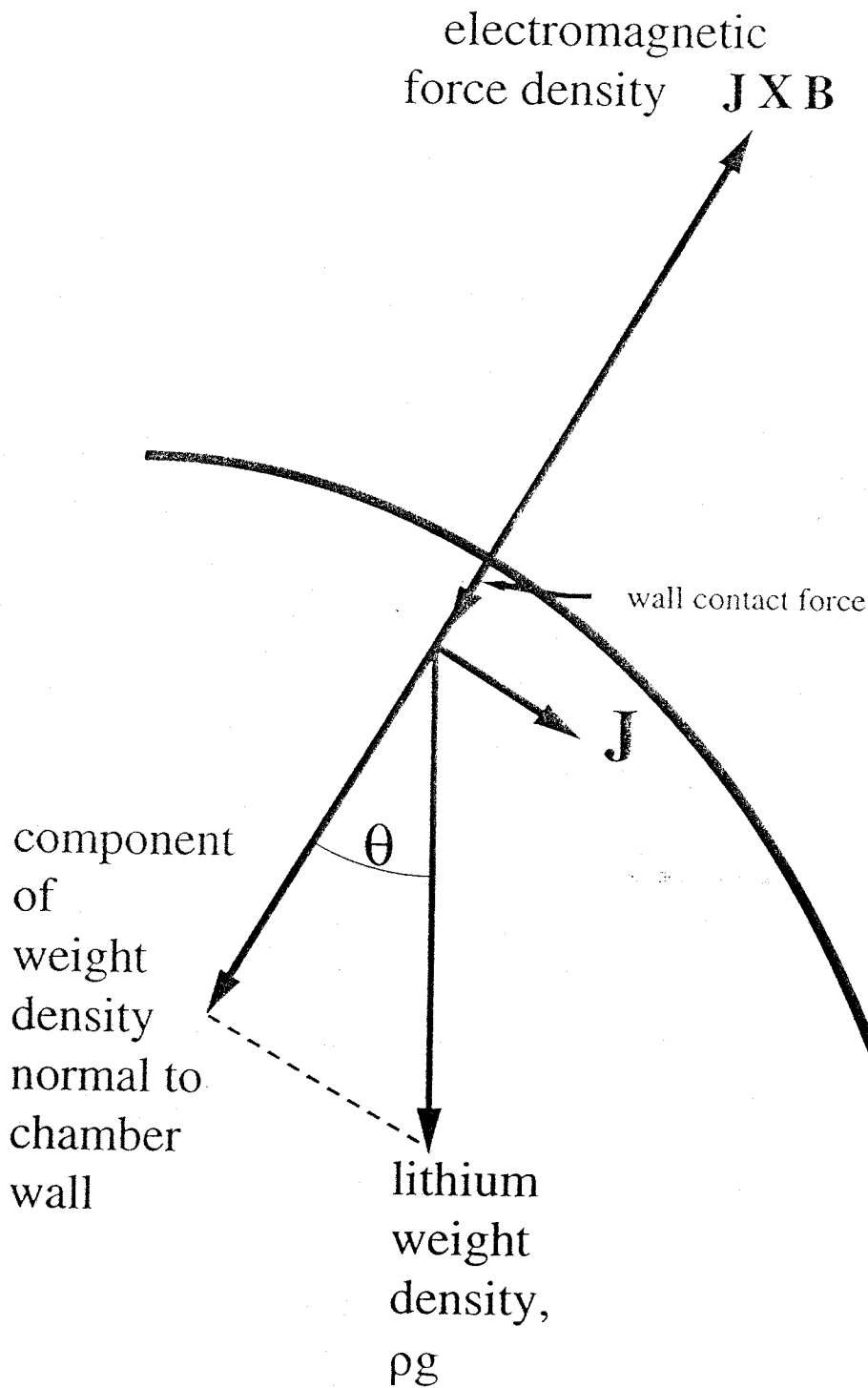
**The two streams are electrically insulated from each other at the top. Poloidal current injected via electrodes is driven through the streams which meet at the bottom of the chamber.**

**The resulting  $\mathbf{J} \times \mathbf{B}$  forces push the streams against the chamber walls away from the plasma.**

# Conceptual Diagram of Liquid Lithium First Wall



# Force Diagram for Liquid Lithium First Wall



Wall Confinement Criterion:

Wall Contact Force  $> 0$ , i.e.

$$|\mathbf{J} \times \mathbf{B}| > \rho g \cos \theta$$

Confinement is guaranteed if

$$J \text{ (amperes/square meter)} > 5047/B$$

(Tesla)

# CLAIMED FLOW FEATURES

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Free surface in vacuum is assumed INSULATING.

FLOW PATH and INJECTED CURRENT follow FLUX SURFACE.

$$\mathbf{B} = \mathbf{B}_p + \mathbf{B}_T$$

$\mathbf{V}$  parallel to  $\mathbf{B}_p$

$\mathbf{J}$  Parallel to  $\mathbf{B}_T$

Thus, No Toroidal Component in  $\mathbf{V}$ , in  $\mathbf{V} \times \mathbf{B}$ , in  $\mathbf{E}$ , in  $\mathbf{J}$ , or in  $\mathbf{J} \times \mathbf{B}$ .

$$\mathbf{V} \times \mathbf{B} = \mathbf{V} \times \mathbf{B}_T$$

$$\mathbf{J} \times \mathbf{B} = \mathbf{J} \times \mathbf{B}_T$$

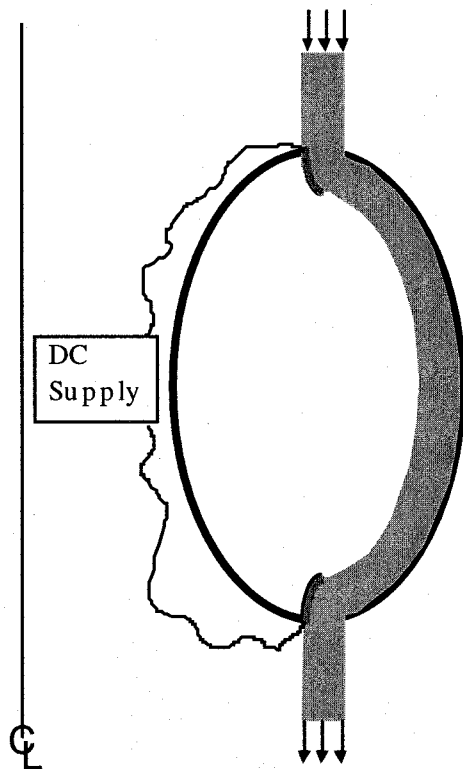
$\mathbf{J} \times \mathbf{B}$  force density is poloidal and perpendicular to  $\mathbf{V}$ .

MHD effects on flow are minimized (since  $\mathbf{V}$  &  $\mathbf{J}$  are perpendicular to the direction of no variation and to the insulating open surface).

## SIMULATION NEED

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**A numerical simulation computer code is needed for engineering investigations of candidate AXISYMMETRIC, FREE SURFACE flows.**



**It should allow changing**

- vessel and electrode geometry**
- liquid inflow rate & pressure**
- electrode voltage**

**It should calculate the free surface shape and the distributions of:**

- electrical currents in the lithium and vessel wall**
- magnetic field**
- the liquid lithium's velocity field**
- the liquid lithium's pressure field**
- transit time, especially at surface**

**It should be economical to develop and use.**

## **SIMULATION DEVELOPMENT**

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**The simulation code must be developed with minimum cost.**

**I have the need to use this simulation in order to properly investigate my proposal of massively liquid lithium walls, and I am developing it myself, as a part-time effort.**

**Existing software modules should be used if that saves effort. Alternatively, published successful numerical algorithms should be used.**

**I will try to have a working simulation before the next APEX meeting.**

**It will be necessary to develop a scheme for validating the simulation.**

**The simulation can also be used to investigate massively liquid lithium schemes for other axisymmetric confinement fusion reactors such as spheromaks, FRCs, RFPs.**

# PHYSICS: VECTOR EQUATIONS & BCs

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Incompressible

$$\nabla \cdot \vec{u} = 0$$

Navier-Stokes:

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = -\frac{\nabla p}{\rho} + \nu \nabla^2 \vec{u} + \vec{g} + \frac{\vec{J} \times \vec{B}}{\rho}$$

Liquid at Free Surface:

$$p = 0$$

Liquid at Material Walls:

$$p > 0; \quad \vec{u} = 0$$

Ampere:

$$\nabla \times \vec{B} = \mu \vec{J}$$

Kirchoff:

$$\Rightarrow \nabla \cdot \vec{J} = 0$$

$$\nabla \cdot \vec{B} = 0$$

Faraday:

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

Ohm:

$$\vec{J} = \sigma(\vec{E} + \vec{u} \times \vec{B})$$

Vector Potential

$$\nabla \times \vec{A} = \vec{B}$$

Coulomb Gauge

$$\nabla \cdot \vec{A} = 0$$

Induction & Electric Field:

$$\vec{E} = -\nabla V - \frac{\partial \vec{A}}{\partial t}$$

Electrode Voltages:

$$V_1 = 0; \quad V_2 = V_{PS}$$

At infinite distance:

$$\vec{A}, \vec{B} \rightarrow 0$$

Note: Driven currents in TF and PF electromagnets influence  $\vec{A}, \vec{B}$ .



## **POSSIBLE DIFFICULTIES AND OTHER REMARKS**

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**It is necessary simulate the unsteady nonlinear dynamics and integrate until reaching a steady-state.**

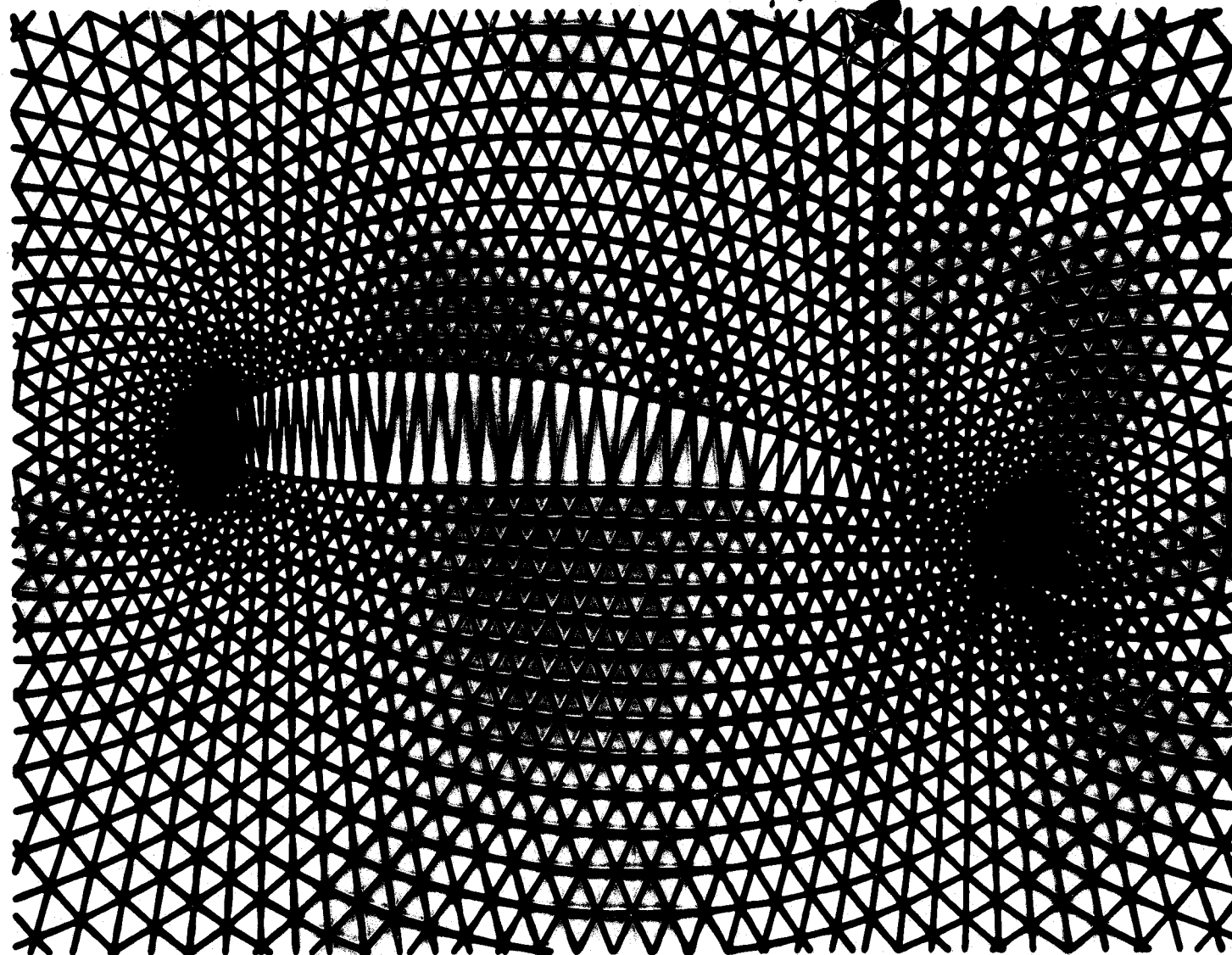
**ANSYS was examined briefly. It may require too many modifications to be an effective starting point. No other existing codes were identified as a good starting point.**

**Galerkin FEM are directly applicable to these PDEs. But axisymmetric fluid flow simulations are less common than 2-D; errors are possible.**

**MHD dynamics will introduce numerical instability possibilities.**

**Important but extremely thin MHD boundary layers can form. A computational grid to resolve them must be capable of having a very small mesh size. Chosen solution will use an adaptive unstructured grid.**

**(I have coded Delauney triangulation of an unstructured grid via Bowyer's algorithm, using quadtrees and linked list data structures for high speed.)**



## **REMARKS (CONT.)**

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A free surface is difficult to model. It's representation may be simplified via adaptive gridpoints which mark and move with the free surface. (Zienkiewicz's FEM text p624 describes such a time-stepping method.)

Incompressible flow is difficult to simulate. Approaches with a published successful track record include:

- (1) Simulating compressibility. (This requires extremely tiny time steps to avoid numerical instabilities due to acoustic waves.)
- (2) The Vorticity-Stream Function method (Never used with free surfaces.)
- (3) The Penalty Function Method. (Requires subtle choices of pressure and velocity finite element interpolation methods to avoid "locking", .)
- (4) Projection Method(s) (Problems unknown. Seems intuitive.)

My initial plans are to try using the Projection Methods.

## PROJECTION METHODS

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These have been successfully applied without MHD coupling ( $\mathbf{J} \times \mathbf{B} = 0$ ).  
The following published algorithm uses explicit Euler integration.

**Step 0: Determine PPE boundary conditions:**

$$\text{At Material Surface: } \frac{\partial p^n}{\partial n} = \rho \{ \nu \nabla^2 \bar{\mathbf{u}}_n^n - (\bar{\mathbf{u}}^n \cdot \nabla) \bar{\mathbf{u}}_n^n \} \quad [\text{Propose } p^n = 0 \text{ @ FS}]$$

**Step 1: Calculate “intermediate velocity field”**

$$\tilde{\mathbf{u}} = \bar{\mathbf{u}}^n + (\Delta t) [ -\nu \nabla^2 \bar{\mathbf{u}}^n + (\bar{\mathbf{u}}^n \cdot \nabla) \bar{\mathbf{u}}^n ] \quad [\text{Propose including } \mathbf{J} \times \mathbf{B} \text{ here}]$$

**Step 2: Solve the “pressure Poisson equation” (PPE)**

$$\nabla^2 p^n = \left( \frac{\rho}{\Delta t} \right) \nabla \cdot \tilde{\mathbf{u}} \quad (\text{with PPE BCs})$$

**Step 3: Correct the “intermediate velocity field”**

$$\bar{\mathbf{u}}^{n+1} = \tilde{\mathbf{u}} - \left( \frac{\Delta t}{\rho} \right) (\nabla p^n - \rho \bar{\mathbf{g}})$$

**Repeat for next time step.**

## **CONCLUSION**

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**I will try to have a working simulation before the next APEX meeting.**

**Your remarks and advice on this effort would be most welcome.**