

The Evolution of Fusion High Power Density

February 1997, San Diego

For experimental devices like ITER, LHD, NSTX and LAR-VNS, we did not worry about neutron wall loading. We felt that the high divertor surface heat flux of about 30 MW/m^2 could be handled by sub-cooled flow boiling of water.

For conceptual reactor designs like ARIES-RS and GA-LAR we reported neutron wall loadings of 4 to 8 MW/m^2 .

We noted the difficulties in the handling of disruption, run-away electrons and type-I ELMs.

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We considered devices like FFHR, Dream, SSTR, GALAR and ST-VNS with neutron wall loadings in the range of 1.5 to 8 MW/m^2 , and divertor heat flux of 2 to 10 MW/m^2 .

Divertor and core radiation are proposed to distribute the transport power to the plasma chamber.

ALPS program presented the grand challenge of having the goal of handling neutron wall loading in the range of $5\text{-}20 \text{ MW/m}^2$ and peak heat flux of up to 50 MW/m^2 .

APEX has a goal of peak neutron wall loading of 7 MW/m^2 , a peak first wall heat flux of 1.5 MW/m^2 , with the suggested fusion goals of neutron wall loading $>10 \text{ MW/m}^2$ and to minimize the peak to average power density.

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APEX indicated goals of peak neutron wall loading $> 10 \text{ MW/m}^2$ and surface heat flux $> 2 \text{ MW/m}^2$.

JAERI demonstrated removal of surface heat flux of 20 MW/m^2 for 10 seconds for 1000 cycles.

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At the peak neutron wall loading of 10 MW/m^2 , APEX/EVOLVE shows a peak nuclear heating of 100 MW/m^3 on the W-alloy and about 30 MW/m^3 on the lithium.

The additional consideration is the actinide burn devices with neutron wall loading in the range of 1 to 3 MW/m^2 and blanket energy multiplication in the range of 10 to 30. These could have a peak and average blanket power density of 100 MW/m^3 and 60 MW/m^3 , respectively, in the blanket material.

Note that we still have not addressed the issues in the handling of disruption, run-away electrons and type-I ELMs.