

# **HELIUM-COOLED REFRACTORY ALLOYS FIRST WALL AND BLANKET-Review**

## **Tasks and leaders**

**Thermal hydraulics**

**C. Wong,**

**C. Baxi**

**Porous First wall Design  
Configuration**

**R. Nygren**

**B. Nelson,**

**P. Fogarty**

**Material compatibility**

**S. Zinkle**

**N. Ghoniem**

**S. Sharafat**

**Helium Impurity control**

**M. Ulrickson**

**Neutronics**

**M. Youssef**

**Activation and afterheat**

**H. Khater**

**Tritium**

**D. K. Sze**

**S. Willms**

**Safety and reliability**

**K. McCathy**

**B. Merrill**

**CCGT**

**R. Schleicher**

**System Study**

**C. Wong**

**APEX-8 meeting, Nov. 8-11, 1999, UCLA**

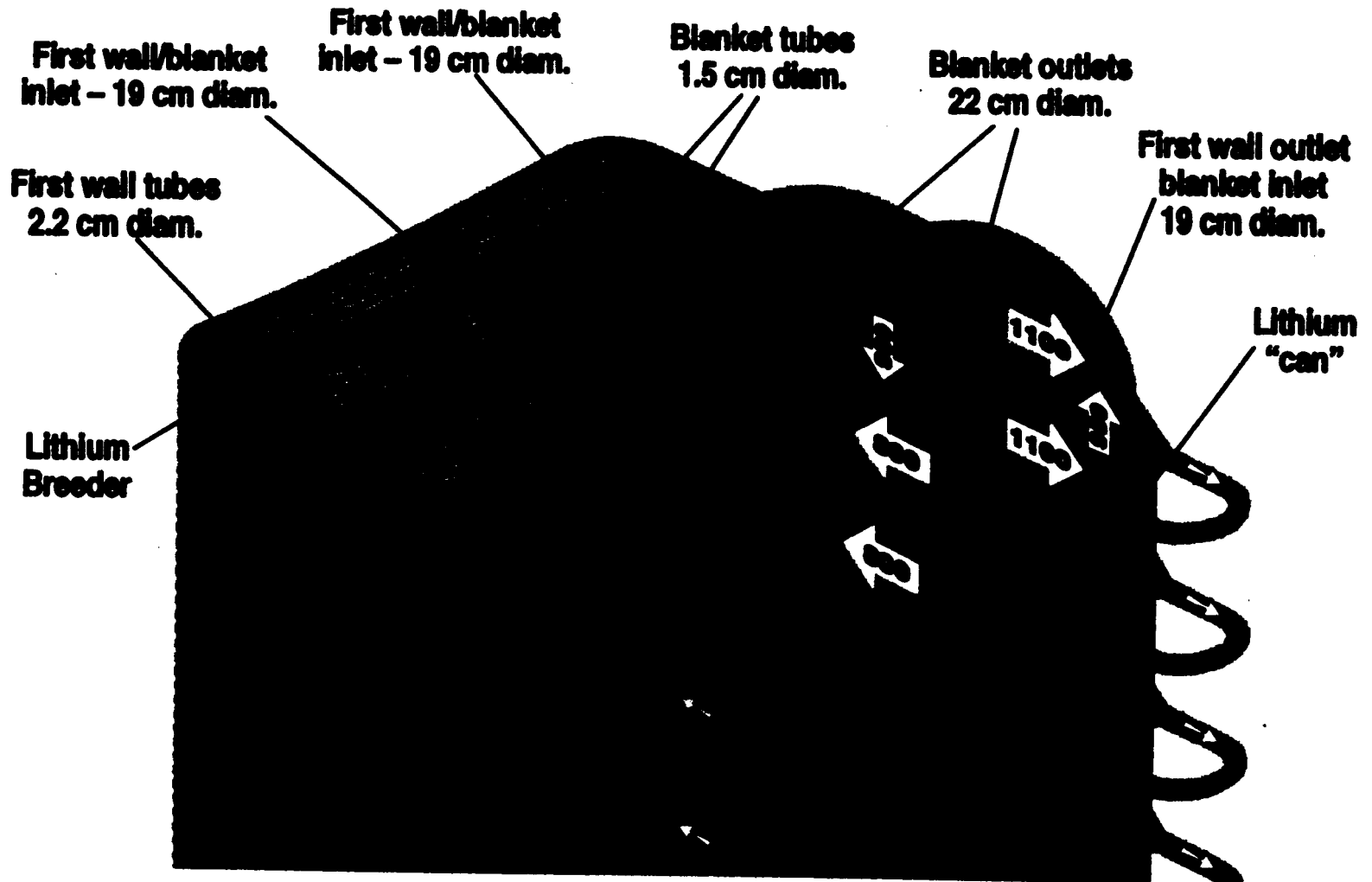
# STRUCTURAL MATERIAL SELECTION AND COMPATIBILITY

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- **Design goal: average neutron wall loading = 7 MW/m<sup>2</sup>, surface heat flux = 2 MW/m<sup>2</sup>, and a peaking factor of 1.4**
- **Ta, Mo, W, Nb and V refractory alloys were evaluated in 1998**
- **W-5Re alloy was selected in 1999 because of projected high temperature performance**
- **The unirradiated mechanical properties of tungsten are strongly dependent on thermomechanical processing conditions. The best tensile and fracture toughness properties are obtained in stress-relieved material**
- **Since data are not available on the possible radiation-enhanced recrystallization of W, and also to account for the presence of welds in the structure, recrystallized mechanical properties were used**
- **W-5Re  $T_{\min} > 800^{\circ}$  was selected to avoid significant increase in the ductile to brittle transition temperature (DBTT)**
- **$T_{\max} < 1400^{\circ}\text{C}$  was selected by consideration of thermal creep, helium embrittlement and oxide formation issues.**

# HELIUM COOLED BLANKET CONCEPT

- One of three "cans" per outboard sector shown with top removed



# POROUS MEDIUM

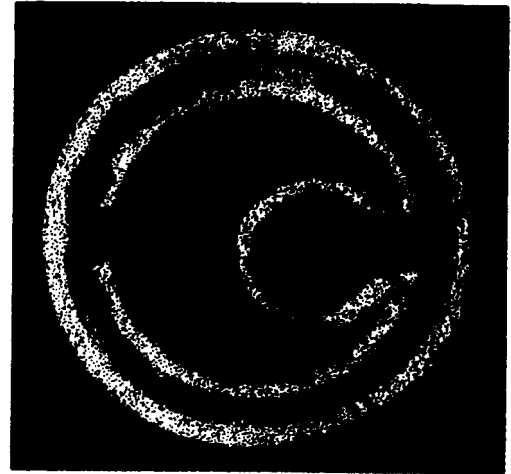
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- **A possible option for the first wall design**

- **Thermacore, Inc. of Lancaster, PA, through grants from DOE's Small Business Innovative Research (SBIR) Program, developed water-cooled and Helium-cooled modules that utilized brazed copper balls as a porous heat transfer medium in copper, Glidcop™ or molybdenum coolant channels.**

- **Their objective was easy-to-fabricate designs for heat sinks that operated at moderate temperature.**

**Thermacore circumferential**



**Thermacore circumferential flow design**

- **Ultramet of Pacoima, CA. Ultramet uses a process in which they build up refractory material with chemical vapor deposition (CVD)**



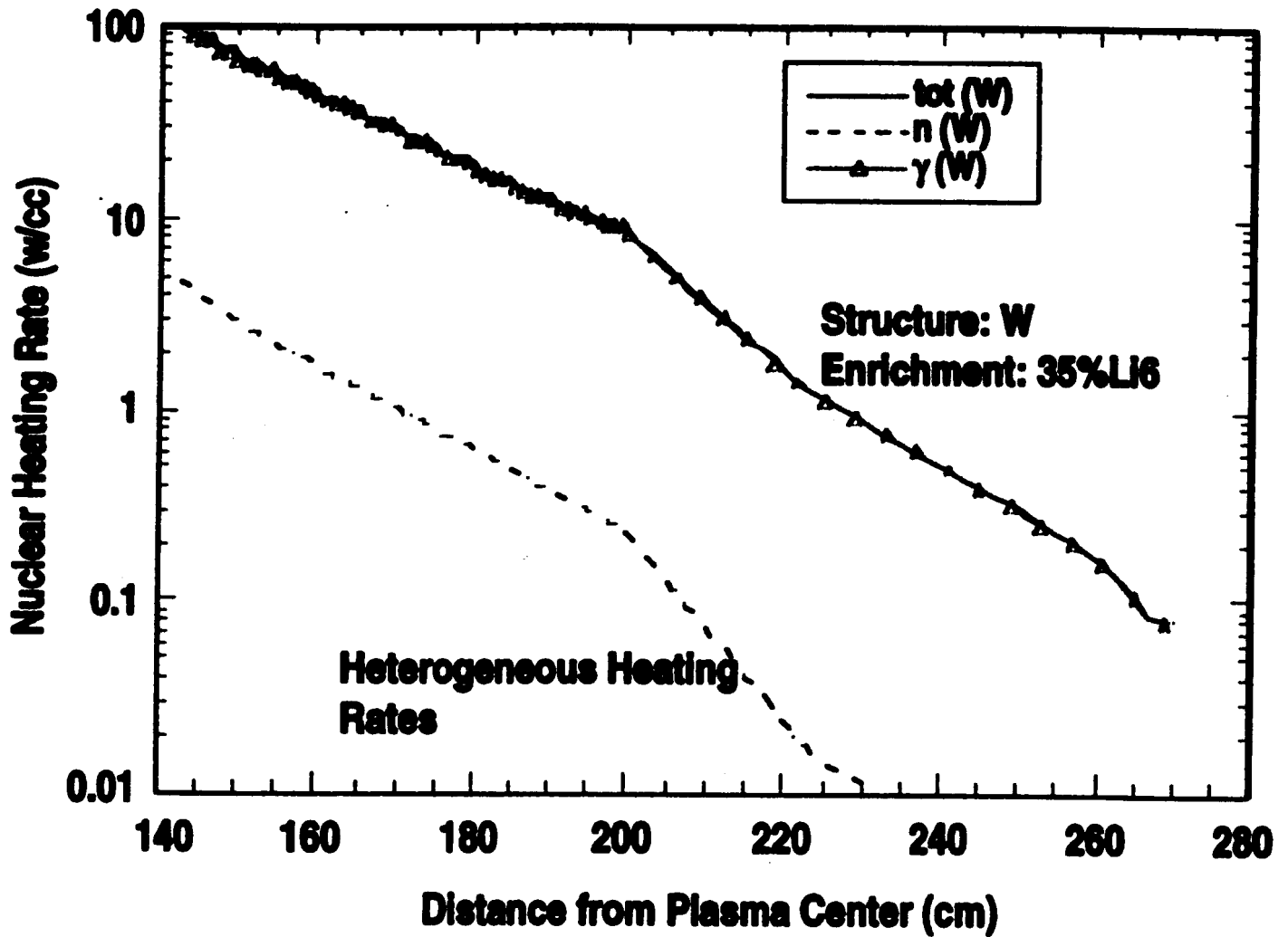
**Porous Ta implant, diam. is 0.75 in.**

# NUCLEAR ANALYSIS

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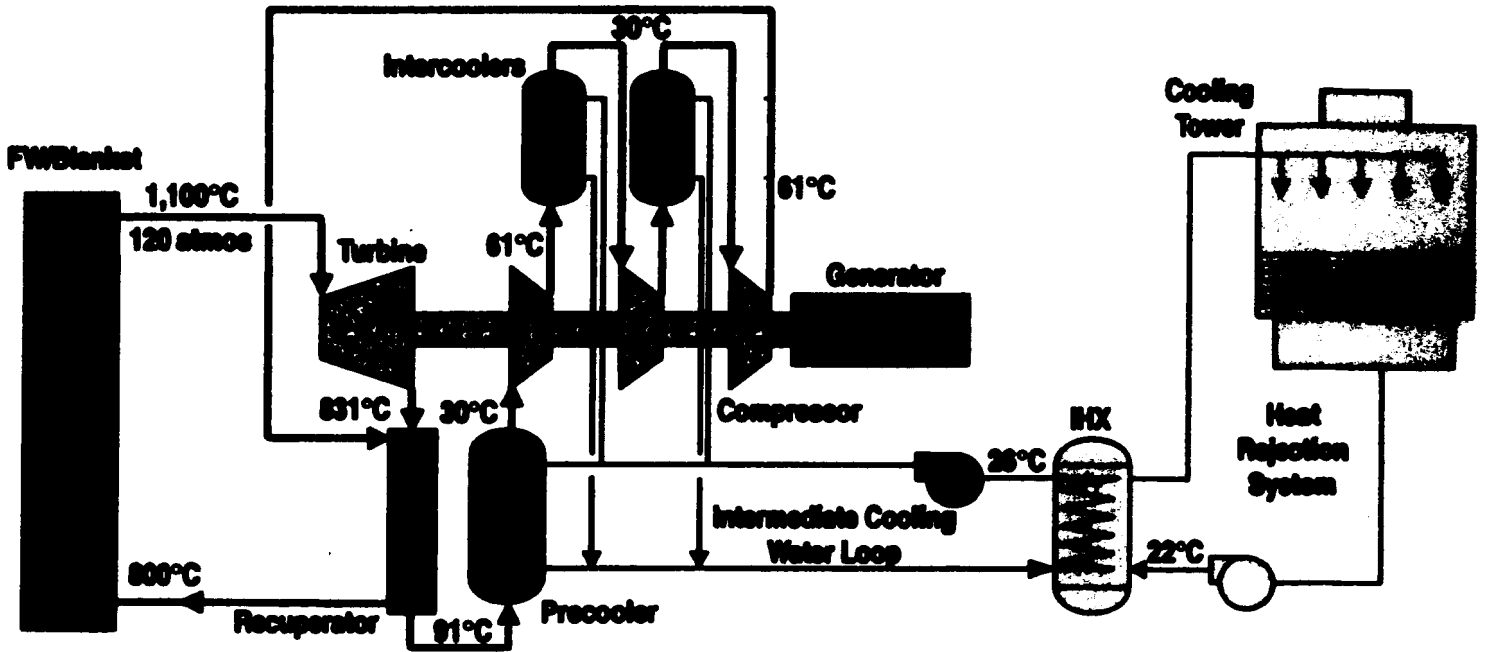
- **Based on the material volume fractions generated, we assessed the impact of W-alloy on: nuclear heating profiles across the blanket, power multiplication, tritium breeding profiles and tritium breeding ratio (TBR), impact of Li-6 enrichment**
- **We assessed the damage indices: DPA, helium, and hydrogen production rates at several key locations, including the vacuum vessel (V.V) and TF coil case**
- **When compared to other refractory alloys like TZM and Nb-1Zr, the best local TBR performance is with W and Li breeder. The TBR increases with Li-6 enrichment and starts to saturate at a value of ~1.43 when Li-6 enrichment is ~35%**
- **The damage parameters, at various locations were estimated in the W-alloy design. Compared to the liquid breeder Filibe, liquid lithium is the less effective material in attenuating the nuclear flux at the V.V. and TF coil by a factor of 6 to 10**
- **The radioactive waste characteristics of different components of the machine were evaluated according to both the NRC 10CFR61 and Fetter waste disposal concentration limits (WDR)**
- **According to Fetter limits, the first wall, module wall, blanket, and transitional zone would not qualify for disposal as Class C waste**
- **The W-5Re alloy produces such a high activity that the first wall would have a WDR more than order of magnitude higher than the Class C WDR limits. (The high WDR is due to the  $^{186m}\text{Re}$ ,  $^{106m}\text{Ag}$ , and  $^{94}\text{Nb}$  isotopes. Only  $^{186m}\text{Re}$  is a product of nuclear interactions with base elements in the W-5Re alloy)**

# TOTAL NUCLEAR HEATING RATES IN THE STRUCTURE



# POWER CONVERSION SYSTEM

## Closed Cycle Gas Turbine (96% recuperator effectiveness was assumed)



Power Conversion System Process Arrangement

# TRITIUM MIGRATION AND CONTROL

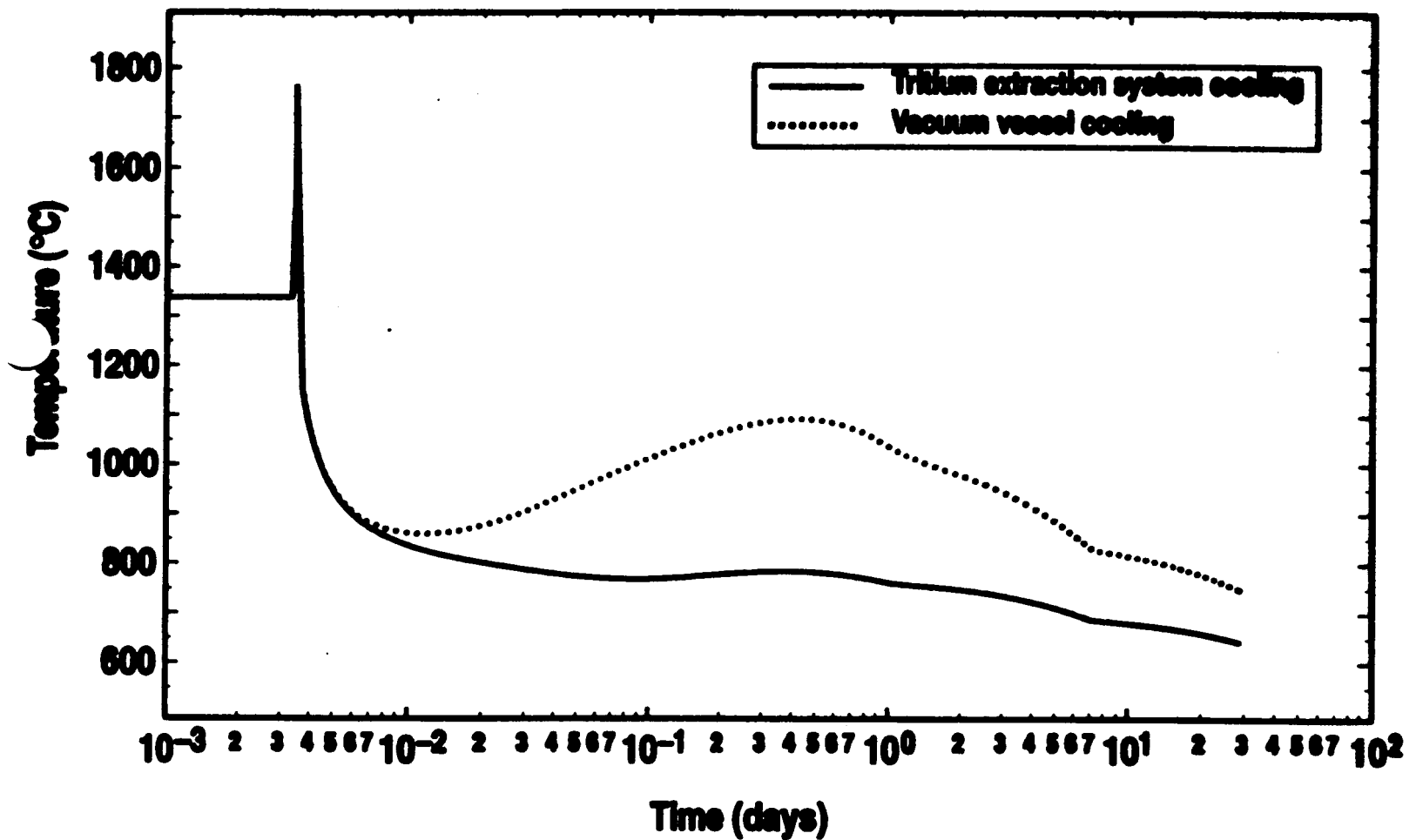
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- **The design goal of the tritium recovery system for lithium is usually to limit the tritium concentration to about 1 appm**
- **This goal is to limit the total tritium inventory in the lithium to less than 200 g**
- **Similar to the ITER design, a cold trap process with protium addition to the lithium is proposed. With the total hydrogen concentration at the saturation limit of 250 appm, the tritium concentration can be below 1 appm**
- **The proposed lithium flow rate for tritium recovery is 20 kg/s. This is a very low flow rate. To maintain uniform tritium concentration, the local flow rate has to be controlled. This design impact will have to be assessed**
- **Recent experimental results from Tritium System Test Assembly show that a permeation window can be used for tritium cleanup from a gas. This process is capable of removing tritium from a gas to ~1 Pa. Since permeation is not a critical issue for this design, 1 Pa tritium partial pressure may be acceptable. The effect of this tritium partial pressure on the operation of the pumps and valves will have to be assessed**



# **FW TEMPERATURE FOR TWO SCENARIOS: VACUUM VESSEL COOLING OPERATES DURING LOCA, AND TRITIUM EXTRACTION SYSTEM OPERATES DURING LOCA**

### **FW Temperature During LOCA**



# CONCLUSIONS

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- **We completed the preliminary design of a high performance He-cooled W-5Re alloy FW/blanket design**
- **A separate first wall that is permitted to flex under heating and a lithium pool configuration was selected**
- **Due to the lack of irradiated data, conservative assumptions on selecting the W-alloy properties have to be used**
- **With regard to the compatibility of W-alloys with oxygen as the primary helium impurity, commercially available solid gettering modules can maintain the impurity level to <1 appm and prevent embrittlement**
- **Potentially, based on the results of selected analyses, the FW/blanket design could meet the material temperature and structural design limits, provided that the peak structural loading during disruptions can be mitigated**
- **The 1-D tritium-breeding ratio of 1.43 can be reached with a Li-6 enrichment of 35%. But the presence of induced radioactivity will not allow the W-alloy components to meet the criteria for classification as low-level waste**
- **W-alloy will generate a high level of afterheat, but with the tritium extraction system operating, long-term accident temperatures remain below 800°C**
- **A cold trap process with added protium to the lithium could be used for tritium extraction**
- **At the CCGT gross thermal efficiency of 57.5%, a super-conducting reactor with an aspect ratio of 4 and an output power of 2 GW(e) is projected to have a COE of 54.6 mill/kWh**

# **Helium-cooled Refractory alloy Design**

## **Proposed next iteration for APEX**

**(To be developed under piggyback mode)**

**“Replace the Li breeder with Filibe”**

### **Motivation:**

**Move away from the chemical reactivity concern of Li**

### **Tasks:**

- **Compatibility**
- **Thermal hydraulics,  $T_{in}/T_{out}=900/1200^{\circ} \text{C}$**
- **Neutronics**
- **Activation/afterheat**
- **Safety**
- **Tritium control**
- **Power conversion**