

Overview

Heat Transfer Issues and Phenomena for Granular First Walls

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HEAT TRANSFER ISSUES

- a. Peak pebble temperature and temperature gradient
 - to ensure temperature and stress limits can be met
- b. Area and volume requirements to transfer heat in the HX
(a high-temperature HX is likely to be expensive)
- c. Temperature distribution, important for other reasons:
 - *e.g.*, tritium control

PHENOMENA

1. Energy deposition characteristics and
temperature evolution in the heated zone
(*low-density free-falling medium*)
2. Heat transfer in the HX
(*dense confined medium*)

R&D NEEDS

1. Energy Deposition

Key Issue:

Deposition characteristics around and through pebbles determines peak surface temperature and near-surface thermal gradients (stresses)

1. Plasma particle flows:

Depends on plasma contact, CX neutral flux

Complications:

Sheath effects

$$\lambda_{\text{Debye}} = 743 T[\text{eV}]^{1/2} n^{-1/2} [\text{cm}]$$

$$100 \text{ eV}, 10^{12} / \text{cm}^3 \rightarrow 75 \mu\text{m}$$

(particle separation less than sheath size would result in electrostatic effects)

Larmor radius effect

$$H \text{ Larmor radius} = 102 T^{1/2} / B [\text{cm}]$$

$$100 \text{ eV}, 50 \text{ kG} \rightarrow 200 \mu\text{m}$$

Pebble rotation

Two reasons this may be worth considering:

1. Determine impact of pebble-plasma contact
2. Important for divertor or near-divertor regions

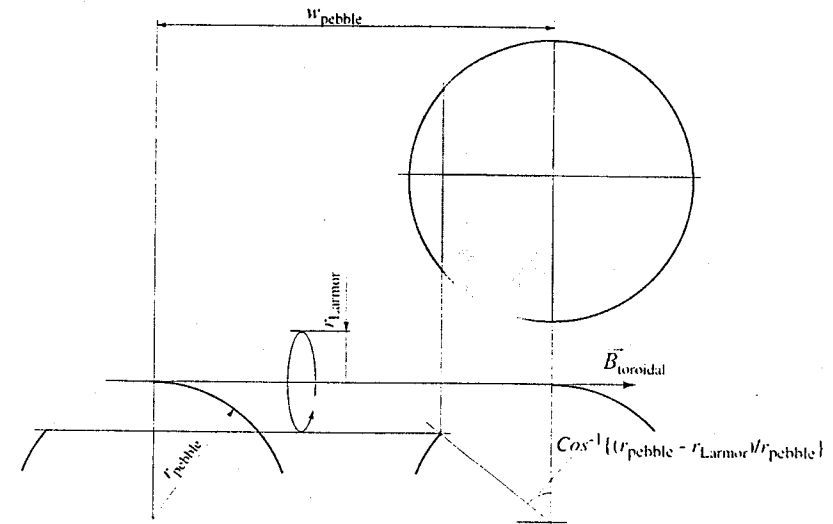


Fig. 1 Larmor radius limited heat load spreading

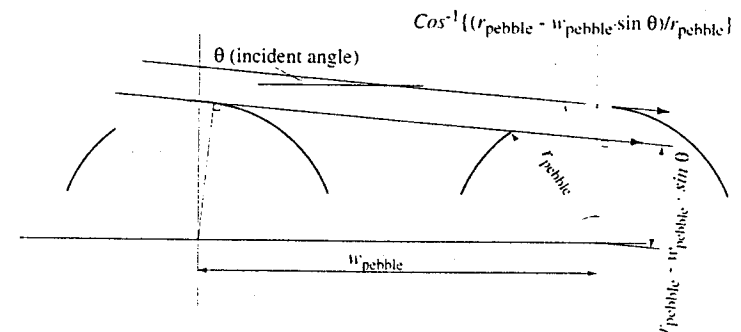


Fig. 2 Incident angle limited heat load spreading

1. Energy Deposition, cont'd.

2. Radiation:

Optical properties depend on geometry, pebble directional emissivity/reflectivity, spectra

Time-dependencies: pebble rotation, bed geometry evolution

Re-emission could reduce temperature peaking factors:

T (C)	$5.7 \times 10^{-8} T^4$
878	0.1 MW/m ²
1000	0.15
1448	0.5
1774	1

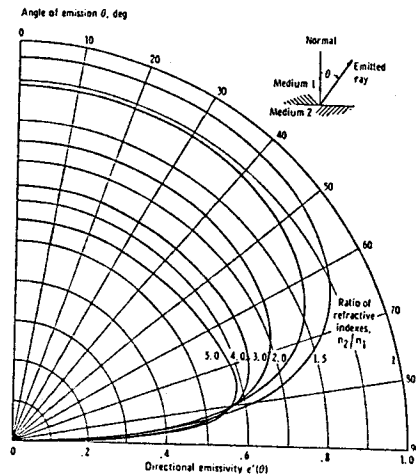
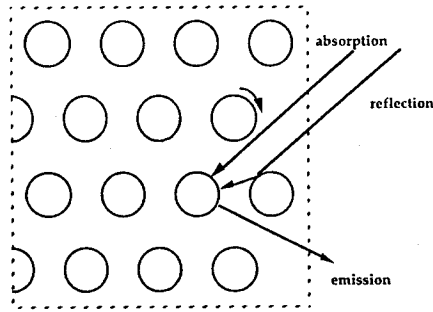


Figure 4-6 Directional emissivity predicted from electromagnetic theory.

2. Heat Transfer in the Heat Exchanger

$$h = h_{pc} + h_{gc} + h_r$$

particle gas radiation
convection* convection

* includes gas-phase conduction at contact points

J. S. M. Botterill, "Fluid-Bed Heat Transfer," Academic Press, London 1975.

- In vacuum, $h_{gc} = 0$
- h_{pc} is highly dependent on the flow field – empirical data typically is used, and can not be extrapolated easily

Key Questions:

1. How is h_{pc} affected by gas pressure?
2. At what point does h_r become dominant?
3. How does h_r reduce h_{pc} ?

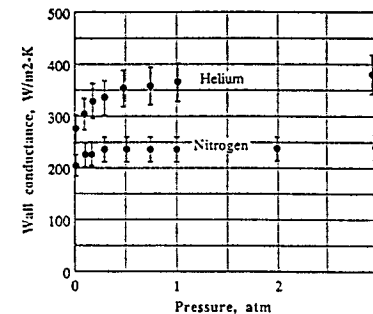


Fig. 8. Wall conductance for 4.3 mm balls with He and N₂ fill gas.

2. Heat Transfer in the Heat Exchanger, cont'd.

$$h_r = \frac{\sigma \epsilon_r (T_{\text{bed}}^4 - T_{\text{surface}}^4)}{T_{\text{bed}} - T_{\text{surface}}}$$

for 1000 C bed, 800 C surface, $\epsilon \sim 1$
 $h_r \sim 400 \text{ W/m}^2\text{-K}$

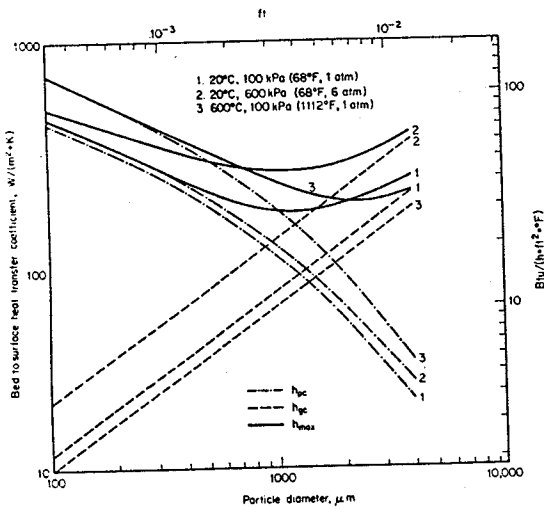


FIG. 9 Effect of particle size on maximum bed-to-surface heat transfer coefficient h_{max} for operation at (1) 20°C and 100 kPa, (2) 20°C and 600 kPa, and (3) 600°C and 100 kPa. Interphase gas convective component of heat transfer h_c taken as that for quiescent bed; particle convective component h_r estimated by difference [26].

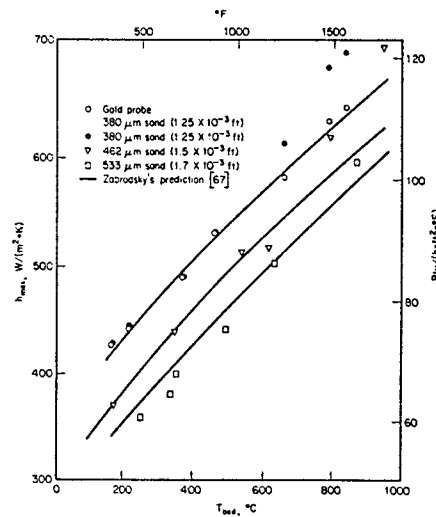


FIG. 10 Variation in maximum bed-to-surface heat transfer coefficient h_{max} with operating temperature compared with the prediction of the Zabrodsky correlation, Eq. (57), for beds of sand of different mean particle size [26]. Note that $h_{\text{max}} \approx h_{p,\text{max}} + h_r$.

Literature

- A huge literature exists on fluidized beds

Limited heat transfer studies in vacuum, vertical free-flow

Some particle-particle and particle-wall radiation results

- 3D numerical simulations and experimental work has been done very recently on the mechanics of granular materials, which is identical under vacuum conditions

X. Zhuang, A.K. Didwania, J.D. Goddard, "Simulation of the quasi-static mechanics and scalar transport properties of ideal granular assemblages," *J. Computational Physics*, 121 (2), Oct. 1995.

V.V.R. Natarajan, M.L. Hunt, E.D. Taylor, "Local measurements of velocity fluctuations and diffusion coefficients for a granular material flow," *J. Fluid Mechanics* 304, Dec. 1995. p.1-25.

C.S. Campbell, "Self-diffusion in granular shear flows," *J. Fluid Mechanics*, 348, 10 Oct. 1997. p.85-101.

- "The heat transfer area seems to be very lightly traveled." I have yet to find an article on vacuum heat transfer in falling beds.

V.V.R. Natarajan, M.L. Hunt, "Heat transfer in vertical granular flows," *Experimental Heat Trans.*, 10 (2), Taylor & Francis, April-June 1997. p.89-107.

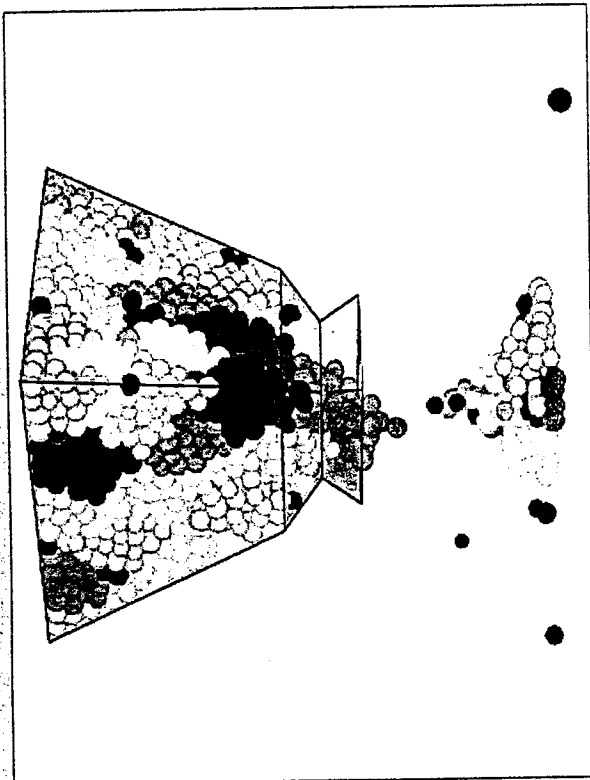
R.E. Nietert, S.I. Abdelk-Khalik, "Thermal hydraulics of flowing particle-bed-type fusion reactor blankets," *Nuclear Eng. & Design*, 68 (3), 1981. p.293-300.

NSF ENGINEERING RESEARCH CENTER on
 Particle Science and Technology (\$60M/11 yr, 1994)
<http://www.erc.ufl.edu/>



ITASCA

Particle Flow Code in 3 Dimensions



A three-dimensional distinct element program to simulate the true 3D behavior of particulate materials. *PFC3D* is the 3D extension of *PFC2D*.

Recommendations

Near-term

- Approximate single-sphere heat transfer and stresses
- 2D (cylinder) model for scoping calculations.
Explore critical issues, develop physics models.
- Plan empirical verification in table-top experiments

Medium-term

- Develop and/or extend an existing 3D code to model energy deposition, heat transfer and stresses.
- Perform table-top experiments

Longer-term

- System development
- Experiments in a plasma device

Collaborations

Japanese activities on granular media for fusion:

Masahiro Nishikawa, Osaka University

Akihiko Shimizu, Kyushu University

Tomoaki Kunugi, Tokai University

US/J meeting on PMI, Yokohama, Oct. 1998